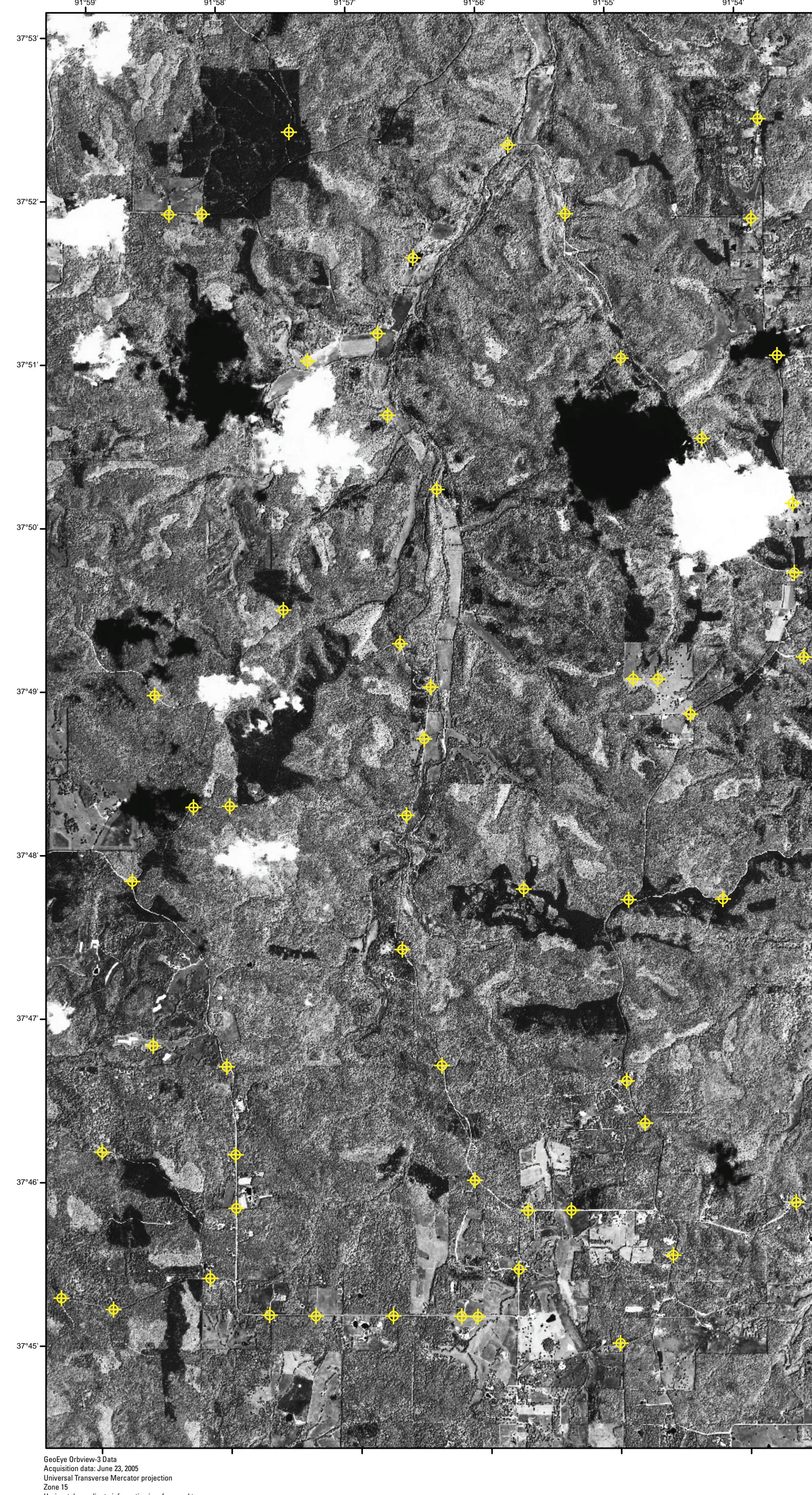


Evaluating the Horizontal Accuracy of GeoEye OrbView-3 Orthorectified Products Over the Kaintuck Hollow, Missouri, Test Site

By Mike Duncan, Brian Fiehler, Michael Starbuck, U.S. Geological Survey, Mid-Continent Geographic Science Center, Rolla, Missouri



Distribution of control points within the Kaintuck Hollow Quadrangle.



Background

The U.S. Geological Survey (USGS) has established procurement contracts to access high-resolution commercial satellite imagery to serve its science, mapping, and homeland security missions, and to provide cost effective centralized procurement services for other government agencies. To ensure that products from these systems can reliably meet USGS and other agency requirements, the USGS has partnered with the National Geospatial-Intelligence Agency and National Aeronautics and Space Administration to combine resources in validating and characterizing high-resolution satellite imagery products of high common interest. This tri-agency partnership is known as the Joint Agency Commercial Imagery Evaluation (JACIE) team. The USGS acquired and tested GeoEye (formerly ORBIMAGE, Inc.) orthorectified panchromatic imagery at 1:24,000-scale acquired on June 23, 2005, over the Kaintuck Hollow, Missouri, test site.

The Independent Control Dataset

Independently surveyed horizontal control points were established on the Kaintuck Hollow, Missouri, quadrangle during the fall of 2002 by the USGS Data Acquisition Response Team (DART). The Global Positioning System (GPS) equipment used to collect data were seven Ashtech Z12 dual-frequency receivers with Ashtech geodetic microstrip antennas, and seven identical fixed-height GPS antenna tripods. The GPS data collection was completed by occupying four National Geodetic Survey control (base) stations, and using three GPS roving receivers to collect the ground control points. Post-processing was performed using Ashtech Prism version 2.4, and adjusted with Ashtech Fillnet version 3.00 to determine the final adjusted positions. This quadrangle and control dataset have been used in previous JACIE horizontal control evaluations.

Testing Methodology

ArcView Geographic Information System software was utilized to display the OrbView-3 image. USGS cartographic technicians used hardcopy orthophoto plots provided by the DART to identify ground control points on the OrbView-3 imagery. Each plot included a magnified view of the control point and a detailed field description. Two technicians, working independently, collected the observed positions for 51 control points in the panchromatic image. The technicians used a zoom factor that enabled the best image measurement for each point. Horizontal differences were calculated between the independent GPS points and the observed image points were displayed. The actual measurements recorded by the two cartographic technicians and the calculated horizontal errors are shown in table 1.

The OrbView-3 imagery used for this test was acquired in June 2005 during leaf-on conditions. Since most of the area in the Kaintuck Hollow quadrangle is heavily forested, some of the GPS control points used in previous horizontal accuracy tests could not be used in this evaluation because of the trees and shadows in the image.

Preliminary Positional Accuracy Results

The test measurements on this image indicate there is a horizontal bias in the image. The simple root mean square error (RMSE) measurement did not work well for this particular orthorectified image because RMSE does not separate the effects of random and systematic error. Instead of calculating RMSE, the results are presented in a manner that attempts to separate the horizontal bias from the random error. To accomplish this, the mean of the differences between the measured points and the control points was calculated for the X and Y directions. This value represents systematic error and provides a simple representation of bias. These values are shown for both cartographic technicians in table 2.

To calculate the standard deviation for the test points while factoring out the systematic error, the following equations were used. This value represents the random error and is shown in table 2.

$$\sqrt{\frac{\sum (X_i - X_{\text{mean}})^2}{n-1}}$$

$$\sqrt{\frac{\sum (Y_i - Y_{\text{mean}})^2}{n-1}}$$

The results indicate the random error is approximately circular and can be approximated by averaging the standard deviations in the X and Y directions. The circular map accuracy standard (CMAS), equivalent to the National Map Accuracy Standard at the 90 percent confidence level is defined as the circular standard deviation multiplied by 2.146. The results of that calculation are shown in table 2.

Table 2. Accuracy Test Results

| OrbView-3 Orthorectified Data | Systematic Error (meters) | | Random Error (meters) | | | |
|---|--------------------------------|--------------------------------|---------------------------------------|---------------------------------------|-----------------------------|--|
| | Mean difference in X direction | Mean difference in Y direction | Standard deviation in the X direction | Standard deviation in the Y direction | Circular standard deviation | Calculated CMAS at 90 percent confidence |
| Panchromatic 1:24,000 Cartographic Technician A | 10.46 | 3.61 | 2.70 | 2.66 | 2.68 | 5.75 |
| Panchromatic 1:24,000 Cartographic Technician B | 10.60 | 3.21 | 3.08 | 3.07 | 3.075 | 6.60 |

The results indicate that the OrbView-3 orthorectified product tested has a systematic shift to the northeast in the observed values compared to the control values. The results also indicate the random error is circular, and can be approximated by averaging the standard deviations in the X and Y directions. Furthermore, the standard deviations for X and Y about the mean error demonstrate that if bias shift is removed, the accuracy of the imagery would be 5 to 7 meters circular error at the 90 percent confidence level. The random error for the image is reasonable, but the systematic error should be investigated further.

Table 1. Data Collected and Horizontal Accuracy Calculations

Cartographic Technician A

| POINT | DESCRIPTION | FIELD X | FIELD Y | REFERRED X | REFERRED Y | AX | AX_Xmean | (AX-Xmean) ² | AY | AY_Ymean | (AY-Ymean) ² | ΔX ² +ΔY ² |
|-----------------------------|-------------|-----------|-----------|------------|------------|-------|----------|-------------------------|------|----------|-------------------------|----------------------------------|
| NE1 CTR OF LOOP | | 418285.59 | 593636.99 | 593373.58 | 418285.02 | 10.58 | -0.05 | 0.00 | 5.44 | 1.83 | 3.33 | 141.56 |
| NE1 RD @ FEET E | | 418244.74 | 593636.97 | 593373.58 | 418244.03 | 10.51 | -0.05 | 0.00 | 5.44 | 1.83 | 3.33 | 113.98 |
| NE1 RD @ DRV 1/2 (S OF 2) | | 418244.74 | 593636.97 | 593373.58 | 418244.03 | 9.85 | -0.61 | 0.37 | 3.45 | 1.16 | 0.02 | 108.93 |
| NE12 RD @ DRV SSW | | 418749.66 | 598053.26 | 598065.46 | 418744.14 | 12.20 | 1.74 | 3.01 | 1.49 | 0.12 | 4.50 | 150.95 |
| NE13 RD @ DRV N | | 418749.66 | 598053.26 | 598065.46 | 418744.14 | 12.20 | 1.74 | 3.01 | 1.49 | 0.12 | 4.50 | 138.53 |
| NE14 TRAIL @ FENCE (CATTLE) | | 418016.60 | 595573.81 | 595588.22 | 418016.46 | 14.41 | 3.95 | 15.57 | 0.05 | -3.56 | 12.64 | 207.54 |
| NE2 RD @ DRAIN | | 419219.20 | 594164.54 | 594175.96 | 419216.36 | 7.42 | -3.04 | 9.22 | 5.97 | 0.36 | 5.56 | 90.72 |
| NE3 RD @ FEET S | | 418972.01 | 593636.97 | 593373.58 | 418972.01 | 10.51 | -0.05 | 0.02 | 5.44 | 1.83 | 3.33 | 113.50 |
| NE4 RD @ TRAIL ENCL-NW | | 418972.14 | 595452.00 | 595463.07 | 418970.15 | 10.16 | -0.30 | 0.09 | 8.01 | 4.40 | 19.34 | 167.44 |
| NE5 RD @ DRV NE | | 418885.28 | 596844.00 | 596852.82 | 418885.07 | 10.51 | -0.55 | 0.33 | 3.45 | 1.16 | 0.02 | 147.57 |
| NE6 RD @ FEET S | | 418733.76 | 593636.97 | 593373.58 | 418733.76 | 11.28 | -0.55 | 0.33 | 5.44 | 1.83 | 3.33 | 122.90 |
| NE7 RD @ DRV ENCL | | 418973.12 | 597206.96 | 597215.44 | 418970.52 | 12.18 | 1.72 | 2.96 | 5.40 | 1.72 | 3.19 | 177.52 |
| NE8 RD @ DRV ENCL | | 418973.12 | 597206.96 | 597215.44 | 418970.52 | 12.18 | 1.72 | 2.96 | 5.40 | 1.72 | 3.19 | 108.85 |
| NE9 RD @ FEET E | | 418973.12 | 597206.96 | 597215.44 | 418970.52 | 12.18 | 1.72 | 2.96 | 5.40 | 1.72 | 3.19 | 97.10 |
| NE10 RD @ FEET W | | 418973.12 | 597206.96 | 597215.44 | 418970.52 | 12.18 | 1.72 | 2.96 | 5.40 | 1.72 | 3.19 | 97.10 |
| NE11 RD @ FEET NW | | 418973.12 | 597206.96 | 597215.44 | 418970.52 | 12.18 | 1.72 | 2.96 | 5.40 | 1.72 | 3.19 | 97.10 |
| NE12 RD @ FEET SW | | 418973.12 | 597206.96 | 597215.44 | 418970.52 | 12.18 | 1.72 | 2.96 | 5.40 | 1.72 | 3.19 | 97.10 |
| NE13 RD @ FEET NE | | 418973.12 | 597206.96 | 597215.44 | 418970.52 | 12.18 | 1.72 | 2.96 | 5.40 | 1.72 | 3.19 | 97.10 |
| NE14 RD @ FEET NW | | 418973.12 | 597206.96 | 597215.44 | 418970.52 | 12.18 | 1.72 | 2.96 | 5.40 | 1.72 | 3.19 | 97.10 |
| NE15 RD @ TRAIL E | | 418973.12 | 597206.96 | 597215.44 | 418970.52 | 12.18 | 1.72 | 2.96 | 5.40 | 1.72 | 3.19 | 97.10 |
| NE16 RD @ FEET SW | | 418973.12 | 597206.96 | 597215.44 | 418970.52 | 12.18 | 1.72 | 2.96 | 5.40 | 1.72 | 3.19 | 97.10 |
| NE17 RD @ FEET NE | | 418973.12 | 597206.96 | 597215.44 | 418970.52 | 12.18 | 1.72 | 2.96 | 5.40 | 1.72 | 3.19 | 97.10 |
| NE18 RD @ FEET NW | | 418973.12 | 597206.96 | 597215.44 | 418970.52 | 12.18 | 1.72 | 2.96 | 5.40 | 1.72 | 3.19 | 97.10 |
| NE19 RD @ FEET SW | | 418973.12 | 597206.96 | 597215.44 | 418970.52 | 12.18 | 1.72 | 2.96 | 5.40 | 1.72 | 3.19 | 97.10 |
| NE20 RD @ FEET NE | | 418973.12 | 597206.96 | 597215.44 | 418970.52 | 12.18 | 1.72 | 2.96 | 5.40 | 1.72 | 3.19 | 97.10 |
| NE21 RD @ FEET SW | | 418973.12 | 597206.96 | 597215.44 | 418970.52 | 12.18 | 1.72 | 2.96 | 5.40 | 1.72 | 3.19 | 97.10 |
| NE22 RD @ FEET NE | | 418973.12 | 597206.96 | 597215.44 | 418970.52 | 12.18 | 1.72 | 2.96 | 5.40 | 1.72 | 3.19 | 97.10 |
| NE23 RD @ FEET SW | | 418973.12 | 597206.96 | 597215.44 | 418970.52 | 12.18 | 1.72 | 2.96 | 5.40 | 1.72 | 3.19 | 97.10 |
| NE24 RD @ FEET NE | | 418973.12 | 597206.96 | 597215.44 | 418970.52 | 12.18 | 1.72 | 2.96 | 5.40 | 1.72 | 3.19 | 97.10 |
| NE25 RD @ FEET SW | | 418973.12 | 597206.96 | 597215.44 | 418970.52 | 12.18 | 1.72 | 2.96 | 5.40 | 1.72 | 3.19 | 97.10 |
| NE26 RD @ FEET NE | | 418973.12 | 597206.96 | 597215.44 | 418970.52 | 12.18 | 1.72 | 2.96 | 5.40 | 1.72 | 3.19 | 97.10 |
| NE27 RD @ FEET SW | | 418973.12 | 597206.96 | 597215.44 | 418970.52 | 12.18 | 1.72 | 2.96 | 5.40 | 1.72 | 3.19 | 97.10 |
| NE28 RD @ FEET | | | | | | | | | | | | |